Tishk International University Engineering Faculty Petroleum and Mining Engineering Department



Petroleum Reservoir Engineering II

Lecture 6: Fundamentals of Reservoir Fluid Flow (III)

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Content:

- Derivation of Darcy's Law for steady-state:
- Linear Flow of Incompressible Fluids
- Linear Flow of Slightly Compressible Fluids
- Linear Flow of Compressible Fluids
- Radial Flow of Incompressible Fluids
- Radial Flow of Slightly Compressible Fluids
- Radial Flow of Compressible Fluids

Linear Flow of Incompressible Fluids:

0.001127 kA (p1 – p2)

 μL

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(1)

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Where q= flow rate, bbl/day

- k= absolute permeability, md
- p= pressure, psia
- μ = viscosity, cp
- L= distance, ft
- A= cross-sectional area, ft^2

Radial Flow of Incompressible Fluids:

 Q_o

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 $\frac{0.00708 \ kh \ (p_e - p_w)}{\mu_0 B_0 \ln(r_e/r_w)}$

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Where $Q_o = \text{oil flow rate, STB/day}$

- p_e = external pressure, psi
- p_{wf} = bottom-hole flowing pressure, psi
- k= permeability, md
- μ_o = oil viscosity, cp
- B_o = oil formation volume factor, bbl/STB
- h= thickness, ft
- r_e = external or drainage radius, ft
- r_w = wellbore radius, ft

- Linear Flow of Slightly Compressible Fluids:
- The relationship that exists between pressure and volume for slightly compressible fluids has been discussed in the previous lecture and is described by following equation:

 $V = V_{ref} [1 + c(p_{ref} - p)]$

The above equation can be modified and written in terms of flow rate as:

$$q = q_{ref} [1 + c(p_{ref} - p)] - - -(3)$$

Where q_{ref} is the flow rate at some reference pressure p_{ref} .

Linear Flow of Slightly Compressible Fluids:

 $q = q_{ref} \left[1 + c \left(p_{ref} - p \right) \right]$

Substituting the above relationship in Darcy's equation gives:

$$\frac{q}{A} = \frac{q_{ref} [1 + c(p_{ref} - p)]}{A} = -0.001127 \frac{k}{\mu} \frac{dp}{dx}$$

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Separating the variables and arranging:

$$\frac{q_{ref}}{A} \int_{0}^{L} dx = -0.001127 \frac{k}{\mu} \int_{p_1}^{p_2} \left[\frac{dp}{1 + c(p_{ref} - p)} \right]$$

- Linear Flow of Slightly Compressible Fluids:
- Integrating gives:

$$q_{ref} = \left[\frac{0.001127 \ kA}{\mu cL}\right] ln \left[\frac{1 + c(p_{ref} - p_2)}{1 + c(p_{ref} - p_1)}\right] - - - (4)$$

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Where q_{ref} = flow rate at a reference pressure p_{ref} , bbl/day

- p_1 = upstream pressure, psi
- p_2 = downstream pressure, psi
- μ = viscosity, cp
- c= average liquid compressibility, psi^{-1}

- Linear Flow of Slightly Compressible Fluids:
- Selecting the upstream pressure p_1 as the reference pressure p_{ref} and substituting in equation (4) gives the flow rate at Point 1 as:

$$q_{1} = \left[\frac{0.001127 \ kA}{\mu cL}\right] ln[1 + c(p_{1} - p_{2})] --- -(5)$$
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- Linear Flow of Slightly Compressible Fluids:
- Choosing the downstream pressure p_2 as the reference pressure and substituting in equation (4) gives:

$$q_2 = \left[\frac{0.001127 \ kA}{\mu cL}\right] ln \left[\frac{1}{1 + c(p_2 - p_1)}\right] - - -(6)$$

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Where q_1 and q_2 are the flow rates at Points 1 and 2, respectively.

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Linear Flow of Slightly Compressible Fluids:

Example 2: A slightly compressible liquid flows in a linear porous media with the following properties:



Calculate the flow rate at both ends of the linear system. The liquid has an average compressibility of $21 * 10^{-5} psi^{-1}$.

Linear Flow of Slightly Compressible Fluids:

Solution:

Choosing the upstream pressure as the reference pressure gives:

 $q_{1} = \begin{bmatrix} (0.001127)(100)(6000) \\ (2)(21 * 10^{-5})(2000) \end{bmatrix} ln[1 + (21 * 10^{-5})(2000 - 1990)]$ ERBIL 2008 $q_{1} = 1.689 \ bbl/day$

Linear Flow of Slightly Compressible Fluids:

Solution:

Choosing the downstream pressure, gives:

$$q_{2} = \begin{bmatrix} (0.001127)(100)(6000) \\ (2)(21*10^{-5})(2000) \end{bmatrix} ln \begin{bmatrix} 1 \\ 1+(21*10^{-5})(1990-2000) \end{bmatrix}$$

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$$q_{2} = 1.692 \ bbl/day$$

• The above calculations show that q_1 and q_2 are not largely different, which is due to the fact that the liquid is slightly compressible, and its volume is not a strong function of pressure.

- Linear Flow of Compressible Fluids:
- For a viscous (laminar) gas flow in a homogeneous-linear system, the real-gas equation of state can be applied to calculate the number of gas moles n at pressure p, temperature T, and volume V:

pV

zRT

• At standard conditions, the volume occupied by the above n moles is given by:

$$V_{sc} = \frac{n z_{sc} R T_{sc}}{p_{sc}} - - -(8)$$

- Linear Flow of Compressible Fluids:
- Combining the above two expressions and assuming $z_{sc} = 1$ gives:

Equivalently, the above relation can be expressed in terms of the flow rate as:

pV

z7

$$\frac{5.615pq}{zT} = \frac{p_{sc}Q_{sc}}{T_{sc}}$$

 $p_{sc}V_{sc}$

 T_{sc}

- Linear Flow of Compressible Fluids:
- Rearranging the previous equation:

 $\left(\frac{p_{sc}}{T_{sc}}\right)\left(\frac{zT}{p}\right)\left(\frac{Q_{sc}}{5.615}\right) = q - - - - (9)$

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Where q= gas flow rate at pressure p in bbl/day

 Q_{sc} = gas flow rate at standard conditions, scf/day

z= gas compressibility factor

 T_{sc} , p_{sc} = standard temperature and pressure in °R and psia, respectively.

- Linear Flow of Compressible Fluids:
- Replacing the gas flow rate q with that Darcy's Law, i.e., equation (1) gives:

$$\frac{q}{A} = \left(\frac{p_{sc}}{T_{sc}}\right) \left(\frac{zT}{p}\right) \left(\frac{Q_{sc}}{5.615}\right) \left(\frac{1}{A}\right) = -0.001127 \frac{k}{\mu} \frac{dp}{dx}$$

- The constant 0.001127 is to convert from Darcy's units to field units.
- Separating variables and arranging yields:

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$$\left[\frac{q_{sc}p_{sc}T}{0.006328 kT_{sc}A}\right] \int_{0}^{L} dx = -\int_{p1}^{p2} \frac{p}{z\mu_{g}} dp$$

- Linear Flow of Compressible Fluids:
- Assuming constant z and μ_g over the specified pressure, i.e., p_1 and p_2 , and integrating gives:

 Q_{sc} =

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 $0.003164T_{sc}A k (p_1^2 - p_2^2)$

 $p_{sc}TLz\mu_{g}$

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Where Q_{sc} = gas flow rate at standard conditions, scf/day

- k= permeability, md
- T= temperature, °R
- μ_g = gas viscosity, cp
- A= cross-sectional area, ft^2

L= total length of the linear system, ft

- Linear Flow of Compressible Fluids:
- Setting p_{sc} = 14.7 psi and T_{sc} = 520 °R in the above expression gives:

 $Q_{sc} = \frac{0.111924Ak \ (p_1^2 - p_2^2)}{TLz\mu_g} - - -(10)$

The above equation is valid for applications when the pressure<2,000 psi. The gas properties must be evaluated at the average pressure \bar{p} as defined below:

$$\bar{p} = \sqrt{\frac{p_1^2 + p_2^2}{2}} - - - -(11)$$

Linear Flow of Compressible Fluids:

Example: A linear porous media is flowing a 0.72 specific gravity gas at 120°F. The upstream and downstream pressures are 2,100 psi and 1,894.73 psi, respectively. The cross-sectional area is constant at 4,500 ft^2 . The total length is 2,500 feet with an absolute permeability of 60md. Calculate the gas flow rate in scf/day ($p_{sc} = 14.7$ psia, $T_{sc} = 520$ °*R*).

- Radial Flow of Slightly Compressible Fluids:
- The relation of pressure and flow rate has been determined previously by following equation:

 $q = q_{ref} [1 + c(p_{ref} - p)]$

If above equation is substituted into the radial form of Darcy's Law:

$$\mathsf{ERB}v = \frac{q}{A_r} = \frac{q}{2\pi rh} = 0.001127 \frac{k}{\mu} \frac{dp}{dr}$$

The following is obtained:

$$\frac{q}{A_r} = \frac{q_{ref} [1 + c(p_{ref} - p)]}{2\pi rh} = 0.001127 \frac{k}{\mu} \frac{dp}{dr}$$

Where q_{ref} is the flow rate at some reference pressure p_{ref} .

Or

- Radial Flow of Slightly Compressible Fluids:
- Separating the variables in the above equation and integrating over the length of the porous medium gives:

$$\frac{q_{ref}\mu}{2\pi kh} \int_{r_w}^{r_e} \frac{dr}{r} = 0.001127 \int_{p_{wf}}^{p_e} \frac{dp}{1 + c(p_{ref} - p)}$$

$$q_{ref} = \left[\frac{0.00708 \ kh}{\mu \ c \ln\left(\frac{r_e}{r_w}\right)}\right] ln \left[\frac{1 + c(p_e - p_{ref})}{1 + c(p_{wf} - p_{ref})}\right]$$

Where q_{ref} is oil flow rate at a reference pressure p_{ref} .

- Radial Flow of Slightly Compressible Fluids:
- Choosing the bottom-hole flow pressure p_{wf} as the reference pressure and expressing the

flow rate in STB/day gives:

$$Q_o = \left[\frac{0.00708 \, kh}{\mu_o B_o c_o \, ln\left(\frac{r_e}{r_w}\right)} \right] \ln\left[1 + c_o(p_e - p_{wf})\right] - - -(5)$$

Where c_o = isothermal compressibility coefficient, psi^{-1}

 Q_o = oil flow rate, STB/day

k= permeability, md

Radial Flow of Slightly Compressible Fluids:

Example: The following data are available on a well in the Red River Field:

 p_e = 2506 psi p_{wf} = 1800 r_e = 745' r_w = 0.25 B_o = 1.25 μ_o = 2.5 $c = 25 * 10^{-6} psi^{-1}$ k = 0.12 Darcyh = 25 ft.

Assuming a slightly compressible fluid, calculate the oil flow rate. Compare the result with that of incompressible fluid.

Radial Flow of Slightly Compressible Fluids:

Solution:

For a slightly compressible fluid, the oil flow rate can be calculated by applying equation (5):

$$Q_o = \left[\frac{(0.00708)(120)(25)}{(2.5)(1.25)(25*10^{-6})\ln(745/0.25)}\right] * \ln[1 + (25*10^{-6})(2506 - 1800)]$$
$$Q_o = 595 STB/day$$

Radial Flow of Slightly Compressible Fluids:

Solution:

Assuming an incompressible fluid, the flow rate can be estimated by applying Darcy's equation,

i.e., equation (2):

 $Q_o = \frac{(0.00708)(120)(25)(2506 - 1800)}{(2.5)(1.25)\ln(745/0.25)}$

 $Q_o = 600 STB/day$

- Radial Flow of Compressible Fluids:
- The basic differential form of Darcy's Law for a horizontal laminar flow is valid for describing the flow of both gas and liquid systems.
- For a radial gas flow, the Darcy's equation takes the form:

where q_{gr} = gas flow rate at radius r, bbl/day r = radial distance, ft h = zone thickness, ft μ_g = gas viscosity, cp p = pressure, psi 0.001127 = conversion constant from Darcy units to field units.

- Radial Flow of Compressible Fluids:
- The gas flow rate is usually expressed in scf/day. Referring to the gas flow rate at standard condition as Q_{g} , the gas flow rate q_{gr} under pressure and temperature can be converted to that of standard condition by applying the real gas equation-of-state to both conditions, or:

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$$\frac{5.615 q_{gr} p}{zTR} = \frac{Q_g p_{sc}}{z_{sc} R T_{sc}}$$
$$\left(\frac{p_{sc}}{5.615 T_{sc}}\right) \left(\frac{zT}{p}\right) Q_g = q_{gr} - -(7)$$

Or

Radial Flow of Compressible Fluids:

 $\left(\frac{p_{sc}}{5.615 \, T_{sc}}\right) \left(\frac{zT}{p}\right) Q_g = q_{gr}$

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Where p_{sc} = standard pressure, psia

- T_{sc} = standard temperature, °R
- Q_g = gas flow rate, scf/day
- q_{gr} = gas flow rate at radius r, bbl/day
- p= pressure at radius r, psia
- T= reservoir temperature, °R
- z= gas compressibility factor at p and T
- z_{sc} = gas compressibility factor at standard condition \approx 1.0

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- Radial Flow of Compressible Fluids:
- Combining equations (6) and (7) yields:

$$\left(\frac{p_{sc}}{5.615 T_{sc}}\right) \left(\frac{zT}{p}\right) Q_g = \frac{0.001127(2\pi rh)k}{\mu_g} \frac{dp}{dr}$$

• Assuming that $T_{sc} = 520$ °R and $p_{sc} = 14.7$ psia:

$$\left(\frac{T Q_g}{k h}\right) \frac{dr}{r} = 0.703 \left(\frac{2p}{\mu_g z}\right) dp - -(8)$$

- Radial Flow of Compressible Fluids:
- Integrating equation (8) form the wellbore conditions $(r_w \text{ and } p_{wf})$ to any point in the reservoir (r and p) gives:

$$\int_{r_w}^r \left(\frac{T Q_g}{k h}\right) \frac{dr}{r} = 0.703 \int_{p_{wf}}^p \left(\frac{2p}{\mu_g z}\right) dp - --(9)$$

- Radial Flow of Compressible Fluids:
- Imposing Darcy's Law conditions on equation (9), i.e.:
- Steady-state flow, which requires that Q_g is constant at all radii

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Homogeneous formation, which implies that k and h are constant

gives:

 $\left(\frac{TQ_g}{kh}\right)\ln\left(\frac{r}{r_w}\right) = 0.703 \int_{p_{wf}}^p \left(\frac{2p}{\mu_g z}\right) dp$

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- Radial Flow of Compressible Fluids:
- The term $\int_{p_{wf}}^{p} \left(\frac{2p}{\mu_g z}\right) dp$ can be expanded to give:

$$\int_{p_{wf}}^{p} \left(\frac{2p}{\mu_{g}z}\right) dp = \int_{0}^{p} \left(\frac{2p}{\mu_{g}z}\right) dp - \int_{0}^{p_{wf}} \left(\frac{2p}{\mu_{g}z}\right) dp$$

Combining the above relationships yields:

$$\left(\frac{TQ_g}{kh}\right)\ln\left(\frac{r}{r_w}\right) = 0.703 \left[\int_0^p \left(\frac{2p}{\mu_g z}\right)dp - \int_0^{p_{wf}} \left(\frac{2p}{\mu_g z}\right)dp\right] - --(10)$$

- Radial Flow of Compressible Fluids:
- The integral $\int_0^p \left(\frac{2p}{\mu_g z}\right) dp$ is called the real gas potential or real gas pseudopressure, and it is usually represented by m(p) or ψ . Thus

$$m(p) = \psi = \int_{0}^{p} \left(\frac{2p}{\mu_g z}\right) dp - --(11)$$

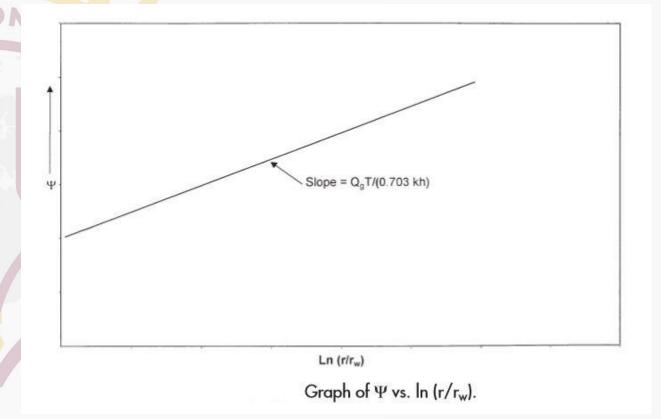
Equation (10) can be written in terms of the real gas potential to give:

$$\left(\frac{TQ_g}{kh}\right)\ln\left(\frac{r}{r_w}\right) = 0.703(\psi - \psi_w)$$

$$\psi = \psi_w + \frac{Q_g T}{0.703 \, kh} \ln \frac{r}{r_w} - - -(12)$$

Or

- Radial Flow of Compressible Fluids:
- Equation (12) indicates that a graph of ψ vs. $ln r/r_w$ yields a straight line of slope $(Q_g T/0.703 \ kh)$ and intercept ψ_w as shown in the figure: ERBIL



- Radial Flow of Compressible Fluids:
- The flow rate is given exactly by:

$$Q_g = \frac{0.703 \ kh(\psi - \psi_w)}{T \ ln \frac{r}{r_w}} - -(13)$$

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• In the particular case when $r = r_e$, then:

$$Q_g = \frac{0.703 \ kh}{r_w} (\psi_e - \psi_w) - - -(14)$$

- Radial Flow of Compressible Fluids:
- The gas flow rate is commonly expressed in Mscf/day, or:

$$Q_g = \frac{kh(\psi_e - \psi_w)}{1422T \ln \frac{r_e}{r_w}} - - -(15)$$

Where Q_g = gas flow rate, Mscf/day

 ψ_e = real gas potential as evaluated from 0 to p_e , psi^2/cp 2008

 ψ_w = real gas potential as evaluated from 0 to p_{wf} , psi^2/cp

k= permeability, md

h= thickness, ft

 r_e = drainage radius, ft

 r_w = wellbore radius, ft